
Hindcast of Typhoon Jebi (2018) storm surge, wave and flood using a coupled model of surge, wave, wave runup and overtopping

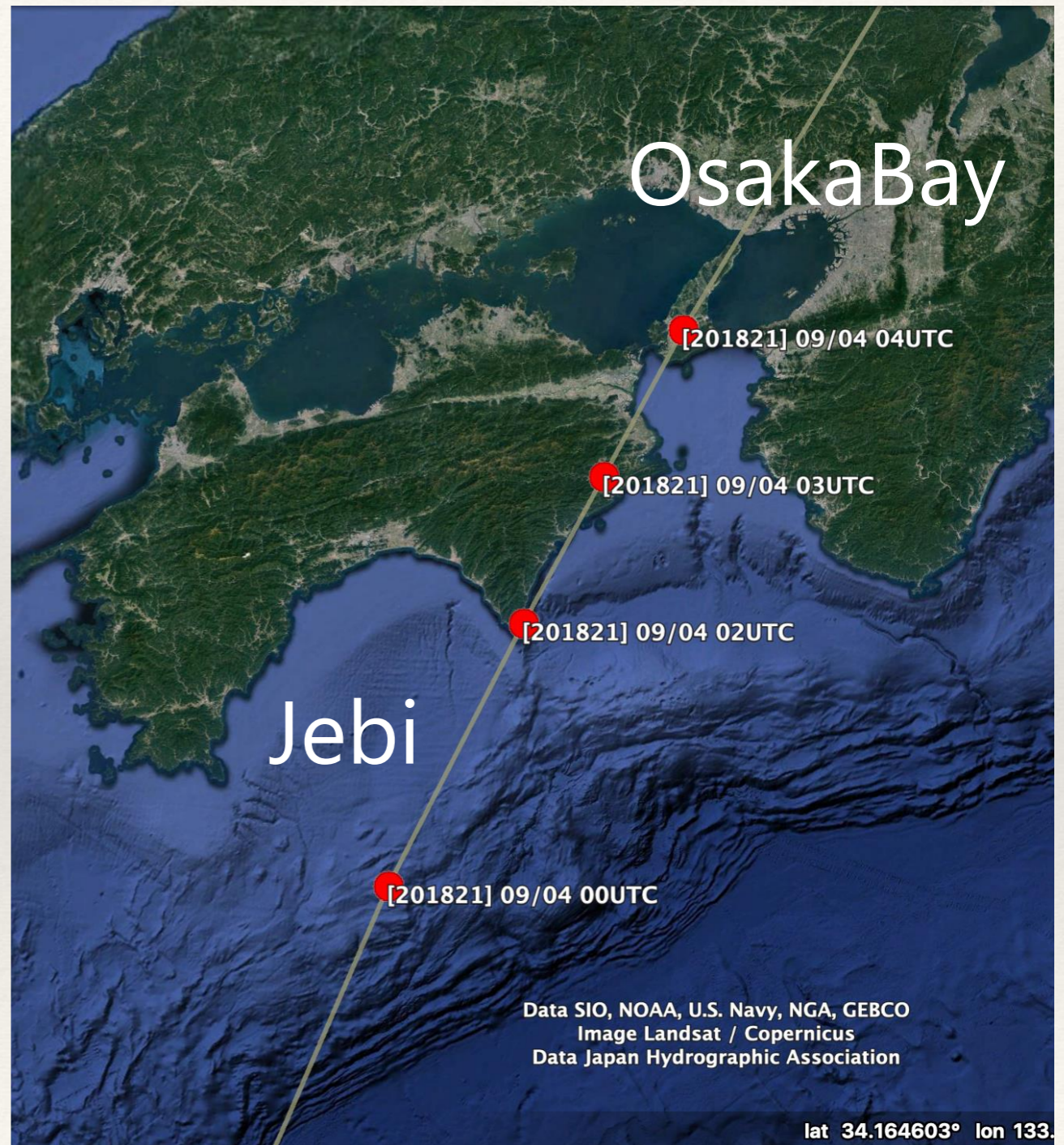
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Tomohiro Yasuda: Kansai University
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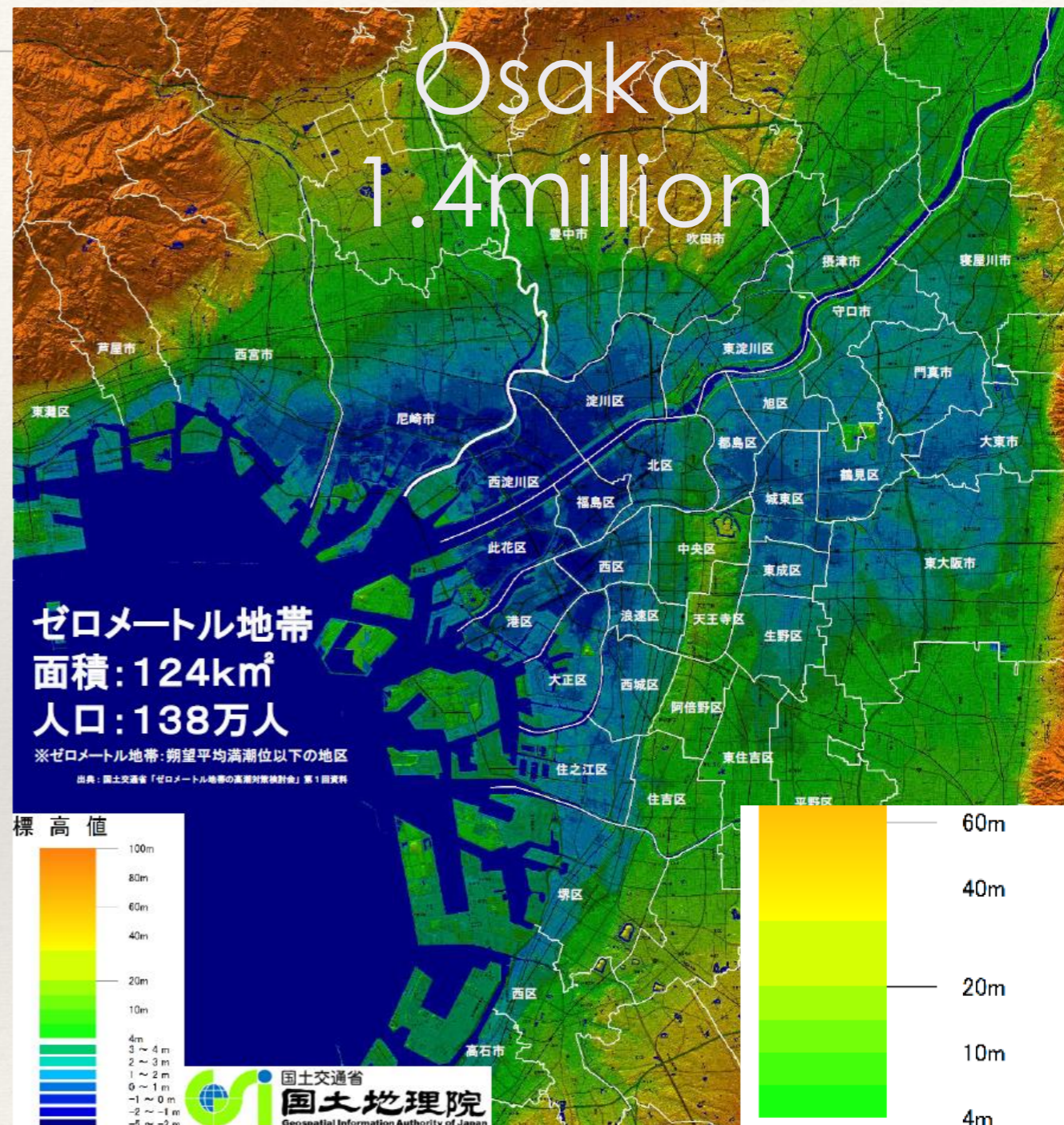
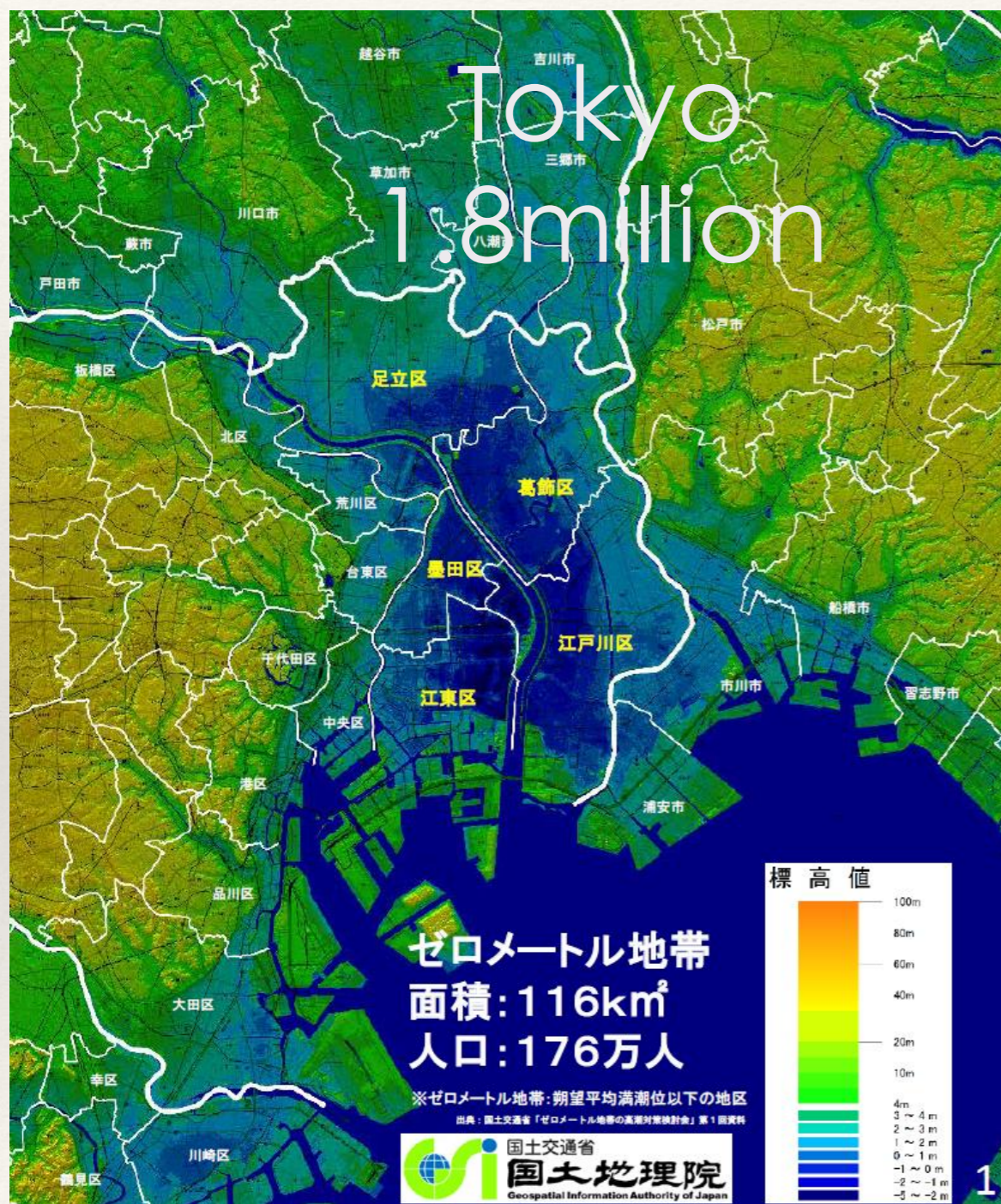
- ❖ Overview
 - ❖ Typhoon Jebi 2018 and its damage
- ❖ Modeling surge, wave and flood
 - ❖ Modeling storm surge and wave in Osaka Bay
 - ❖ Flooding at Kansai Airport

Overview of Typhoon Jebi 2018

- ❖ The most catastrophic tropical cyclone in Japan for five decades
 - ❖ since Typhoon Nancy (1961) (so call 2nd Muroto Typhoon)
- ❖ Landfall on the west coast of Osaka Bay
- ❖ historical record-breaking wave and surge heights in the inner bay
 - ❖ max. sea level: **3.29** m
 - ❖ max. surge level: **2.78** m
 - ❖ max. significant wave: **4.72** m



Exposure is extremely high below the sea level



Summary of damage

被害の概要



Storm surge barriers in Osaka TC Jebi 2021

2018.9.4 台風21号 木津川水門



Storm surge run-up river

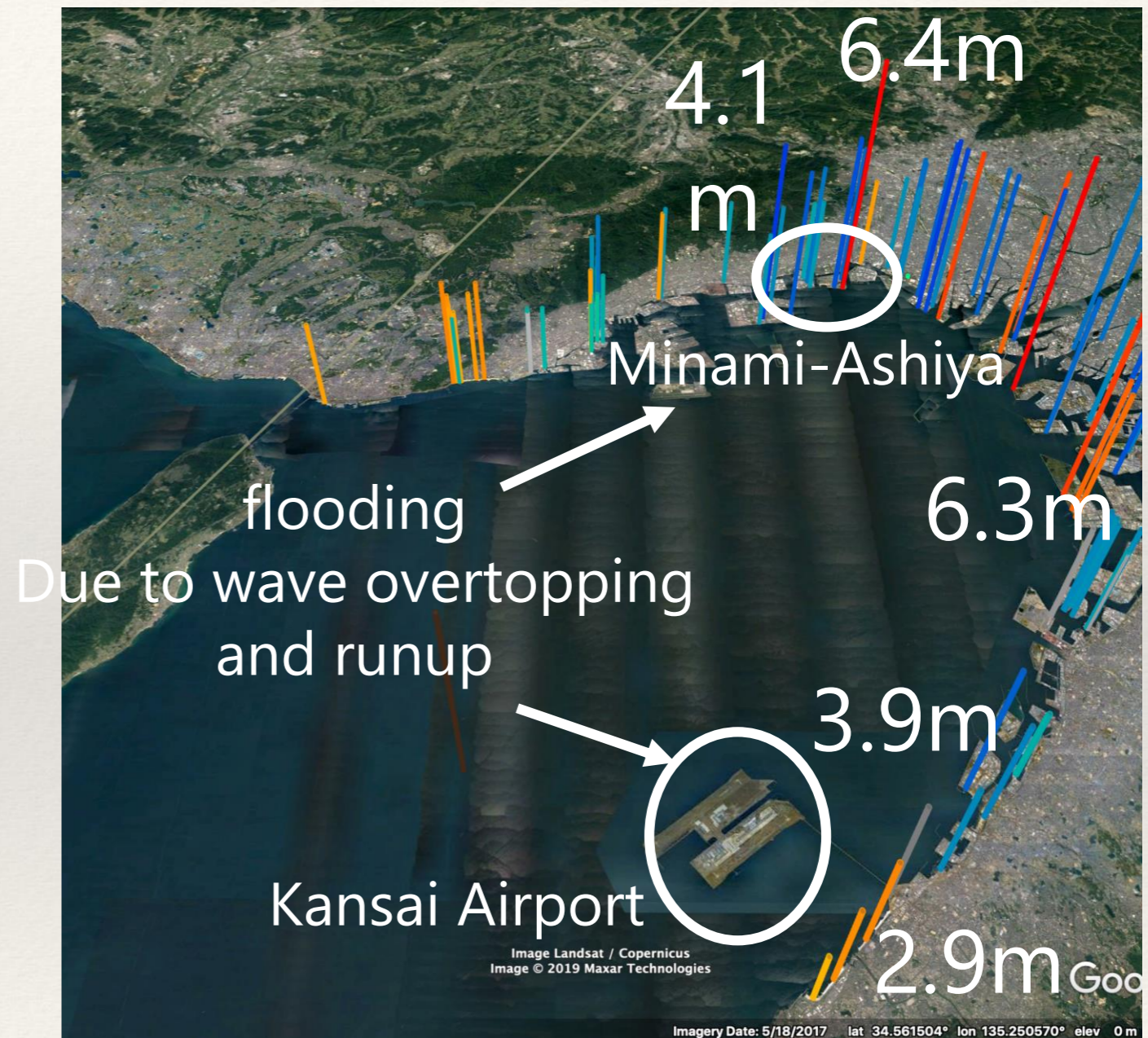


Inundated Kansai Airport



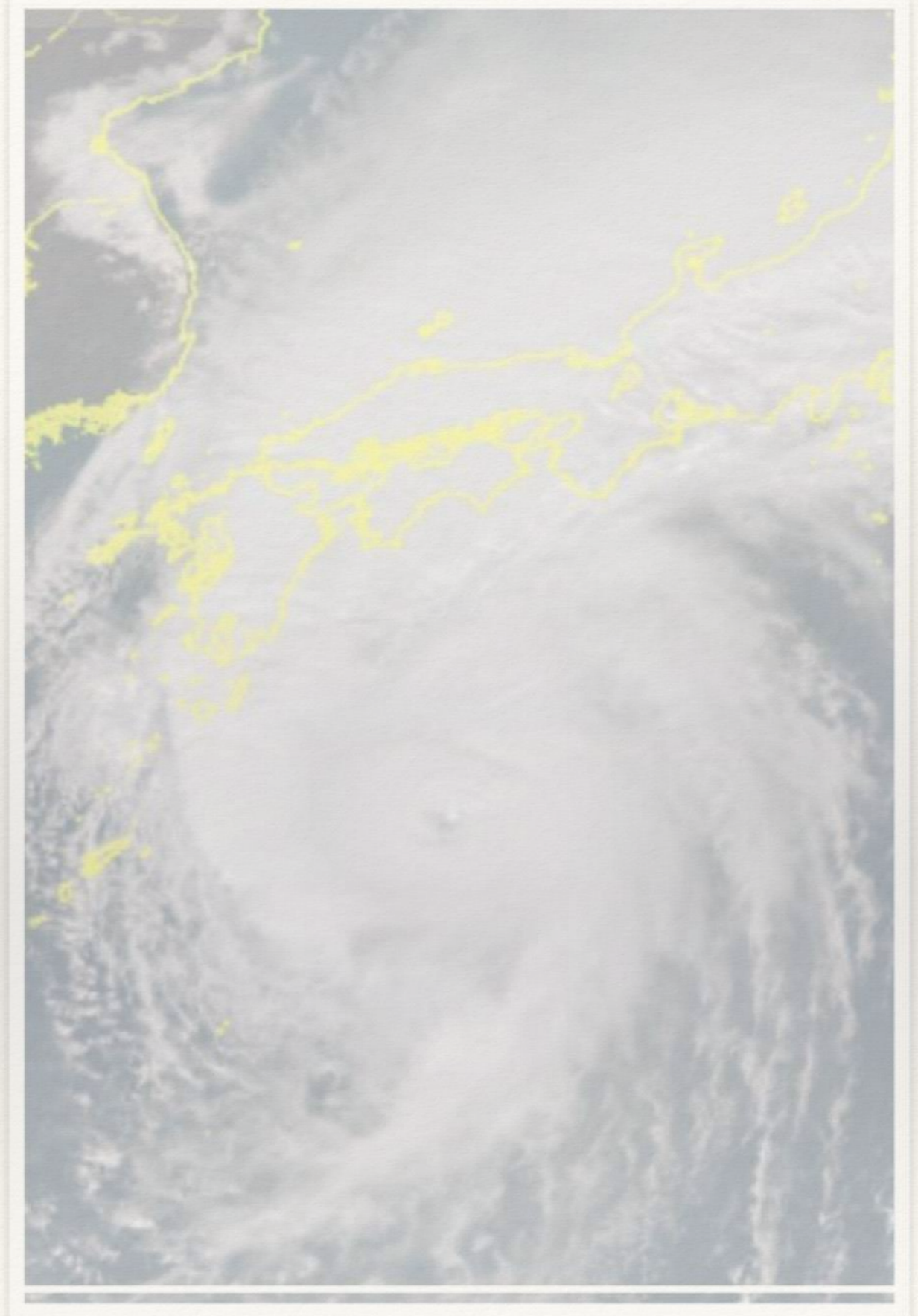
Survey results of flooding depth

- ❖ 39 academics at 14 universities and 2 institutes supported by JSCE
 - ❖ coastal flooding mostly due to wave runup and overtopping
 - ❖ flooding depth: more than 6 m
- ❖ Survey data: freely available
 - ❖ <http://www.coastal.jp/ja/>
 - ❖ 2018 Typhoon Jebi Post-Event Survey of Coastal Damage in the Kansai Region, Japan in Coastal Engineering Journal



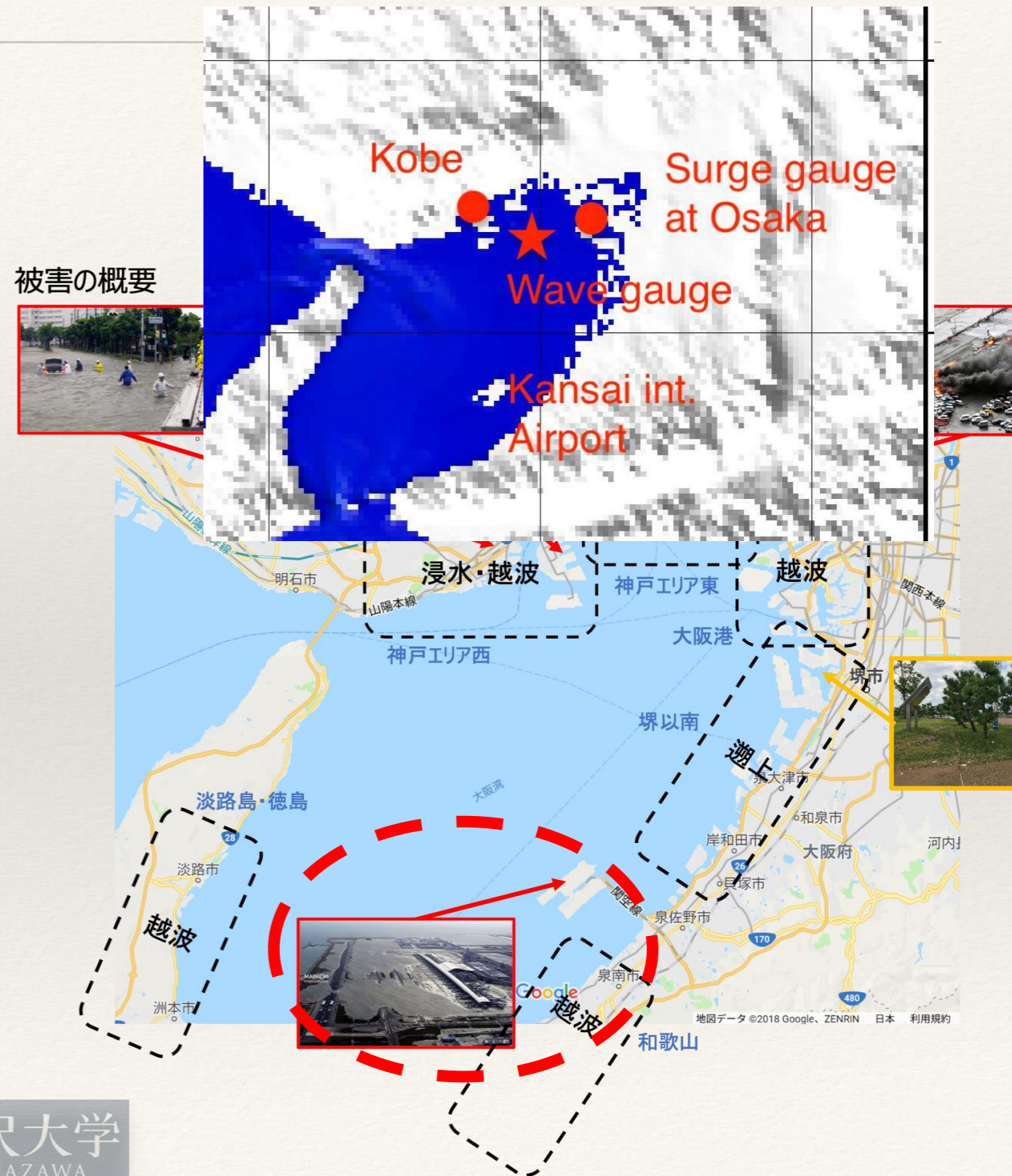
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Modeling storm surge and wave in Osaka Bay



Hindcasting surge and wave

- ❖ Coupled model of surge, wave and tide (SuWAT, Kim et al. 2015)
 - ❖ A wave dependent drag coef.
 - ❖ Wave radiation stress
 - ❖ Five nested domains downscaling 7,300 m to 90 m
- ❖ Forcing
 - ❖ WRF hindcast
 - ❖ Parametric TC model

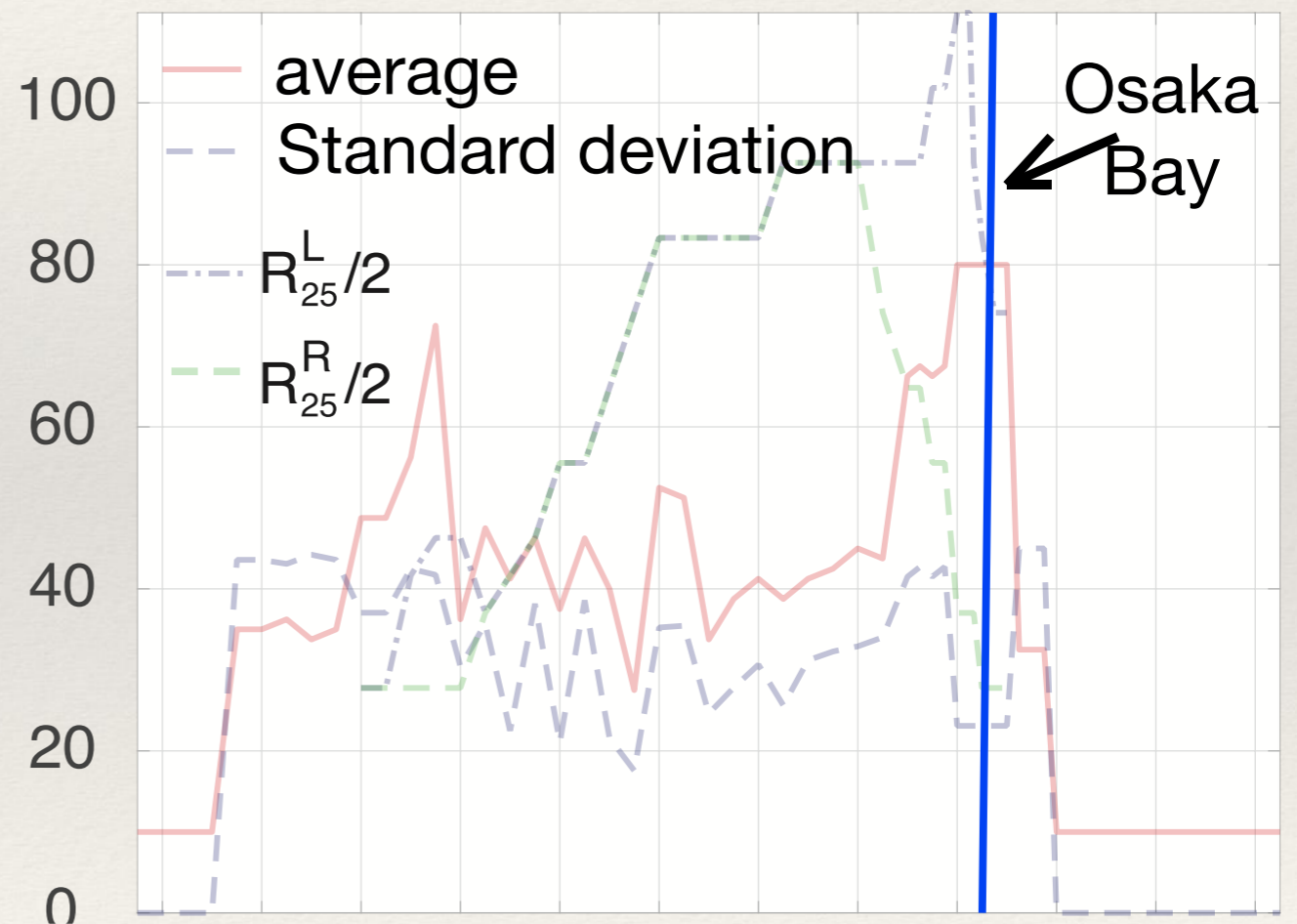


Tuning parametric TC model for this event

- ❖ Saturation of momentum transfer coefficient C_D in high wind speed region
- ❖ Typhoon's feature in the bay
 - ❖ Strongly asymmetry wind field above the bay
- ❖ Similar work for TC Haiyan 2013
 - ❖ Kim et al. (2015) Ocean Dyn.

Wu (1982):

$$C_D = \begin{cases} 1.2875 \times 10^{-3} & \text{for } U_{10} < 7.5\text{m/s} \\ (0.8 + 0.065U_{10}) \times 10^{-3} & \text{for } U_{10} > 7.5\text{m/s} \end{cases}$$

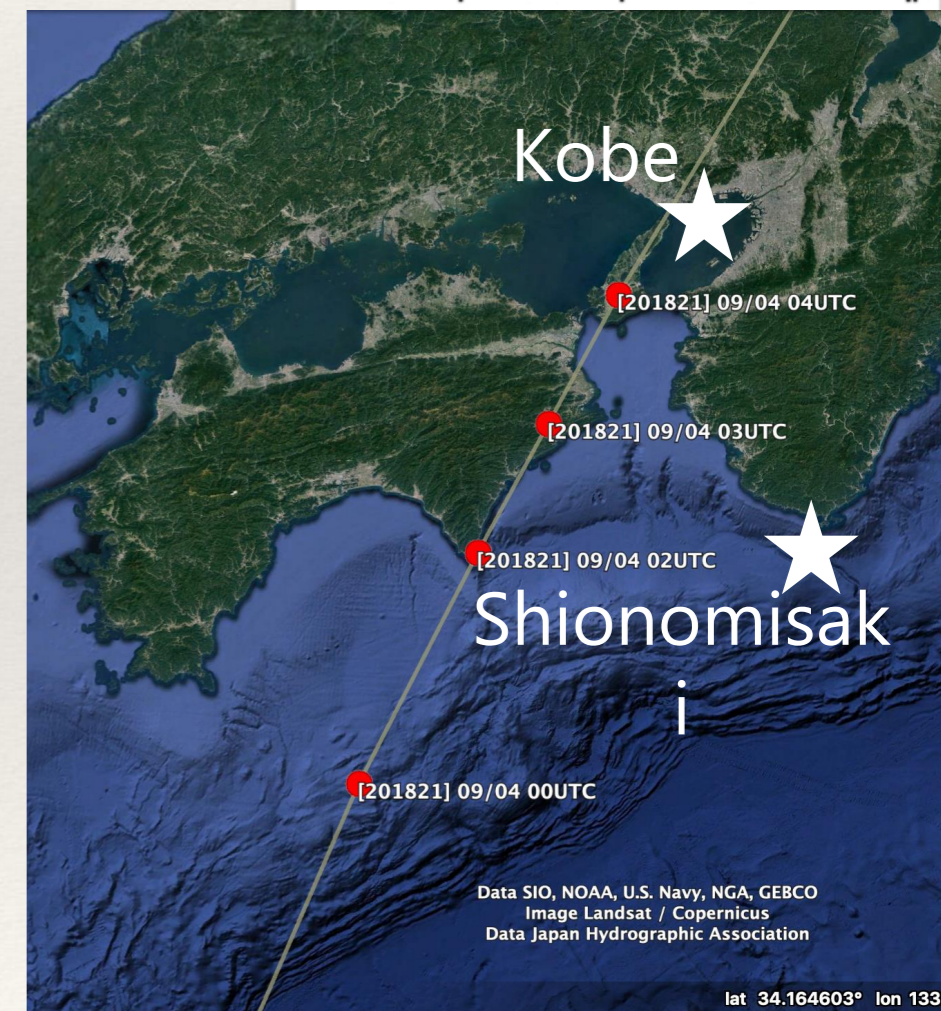


Average radius : 80 Km from satellite images
Radius on the right-hand side: 35 Km

2. Sensitivity of Rmax

- ❖ Rmax in the bay = 35, 40, 50, 60, 70, 80km
- ❖ Wind limit at 20, 25, 30 m/s

Case	R_{\max} (km)	Wind limit
1	30	25
2	35	20, 25, 30
3	40	20, 25, 30
4	50	20, 25, 30
5	60	20, 25, 30
6	70	20, 25, 30
7	80	20, 25, 30



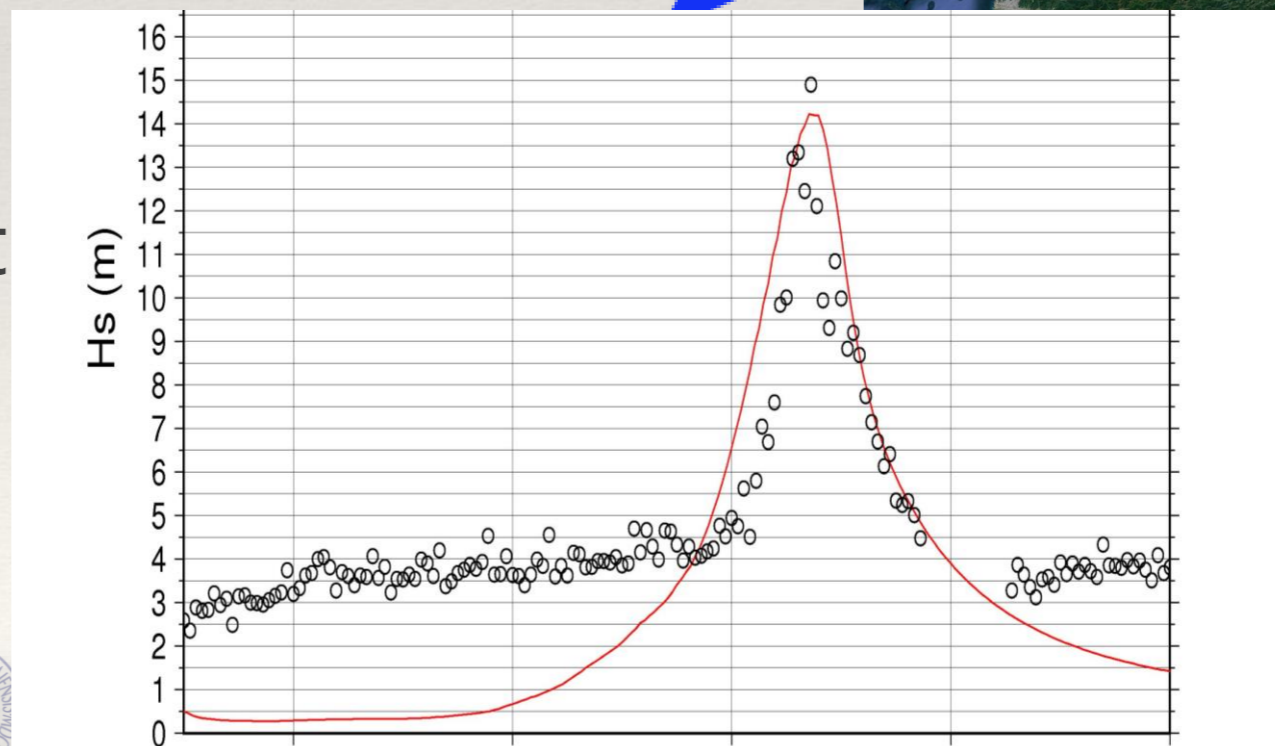
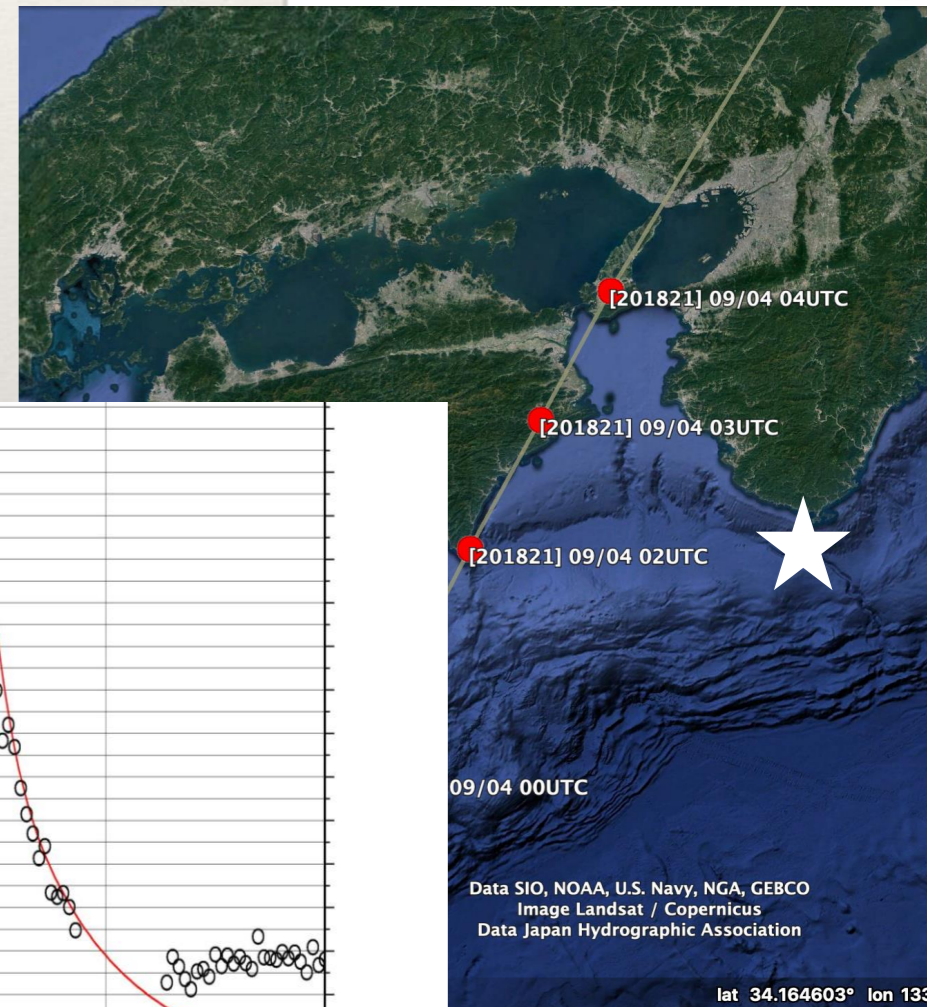
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2. Sensitivity of Rmax with wind limit

- ❖ Rmax in the bay = 35, 40, 50, 60, 70, 80km
- ❖ Wind limit at 20, 25, 30 m/s

Case	R_{max} (km)	Wind limit
1	30	25
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Wind limit at 25 m/s
at Shionomisaki

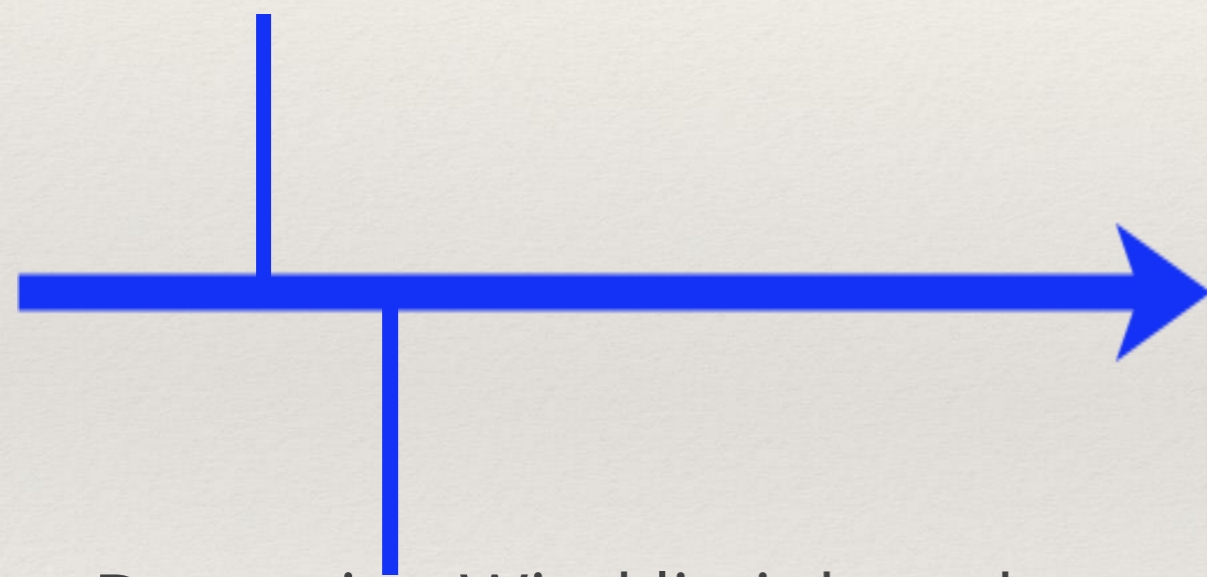


- ❖ Determine Wind limit based on Hs at Shionomisaki and Kobe

Select 25 m/s

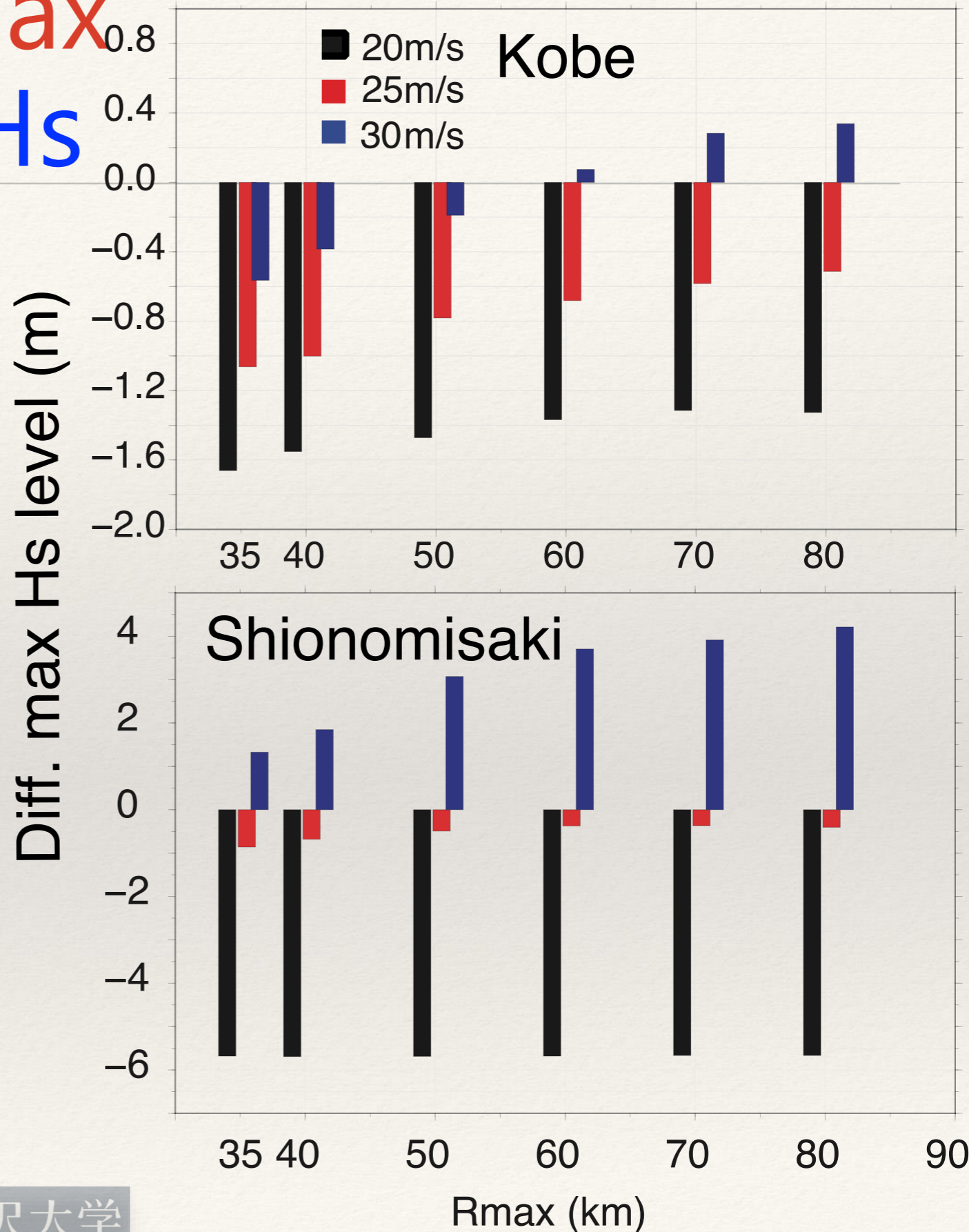
2. Sensitivity of Rmax with wind limit to Hs

- ❖ Rmax in the bay = 35, 40, 50, 60, 70, 80km
- ❖ Wind limit at 20, 25, 30 m/s



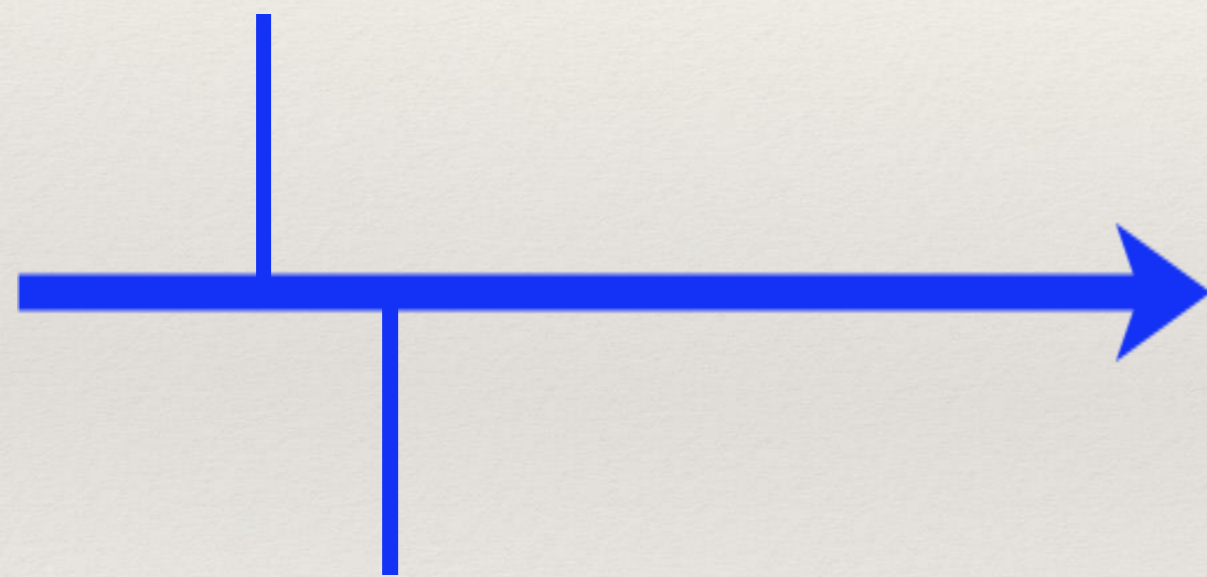
- ❖ Determine Wind limit based on difference between observed and calculated Hs levels at Shionomisaki and Kobe

25 m/s selected



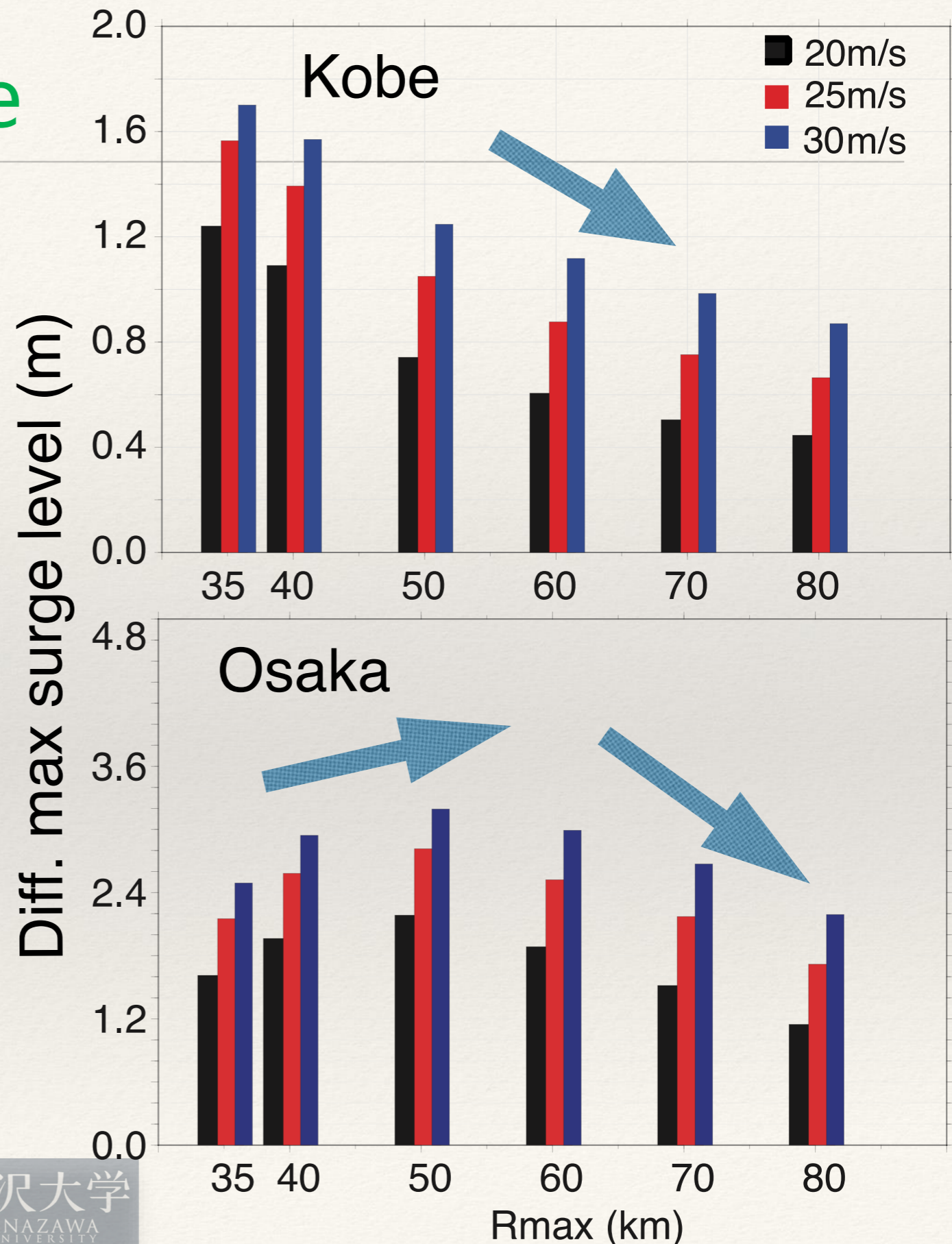
2. Sensitivity of Rmax with wind limit to surge

- ❖ Rmax in the bay = 35, 40, 50, 60, 70, 80km
- ❖ Wind limit at 20, 25, 30 m/s



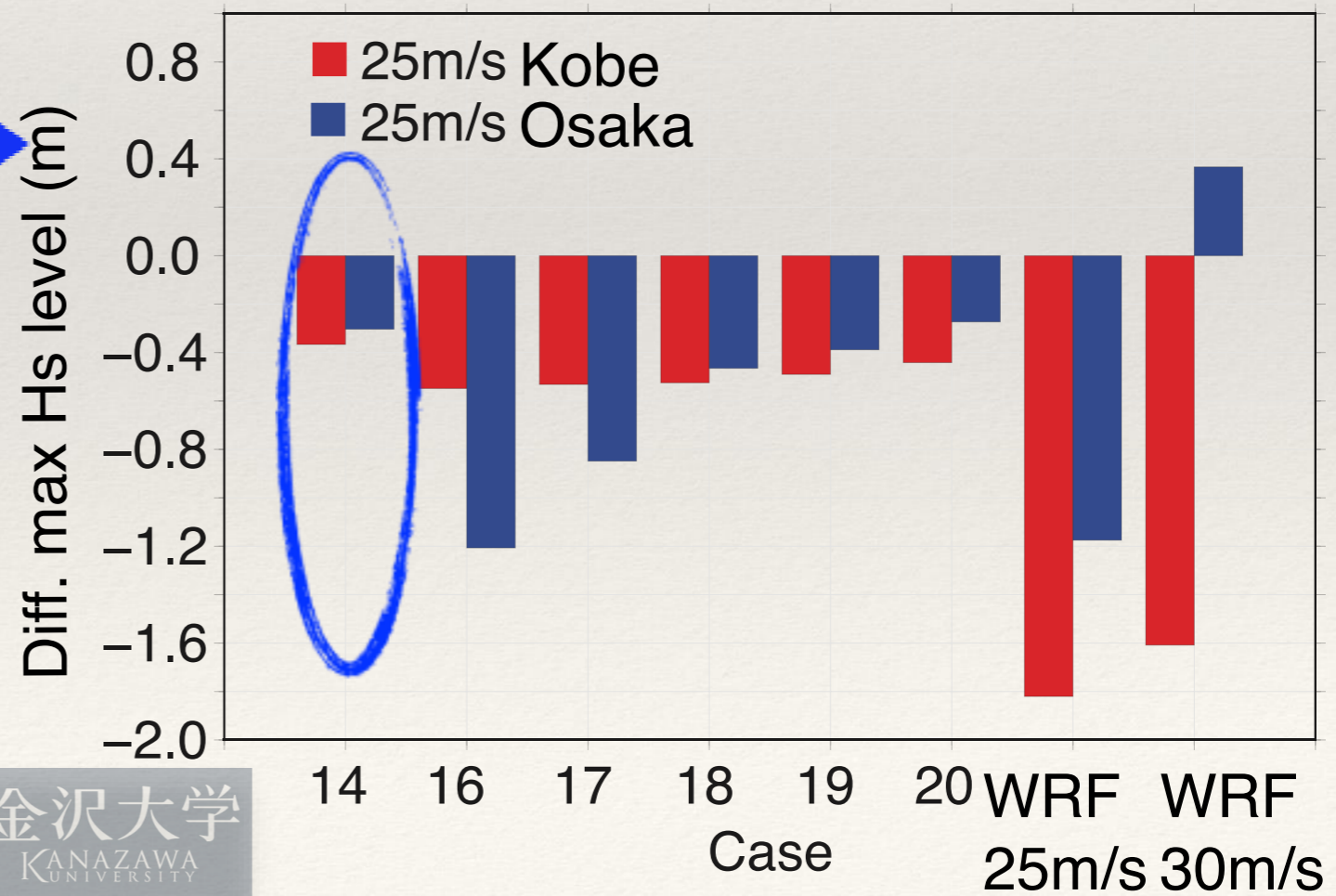
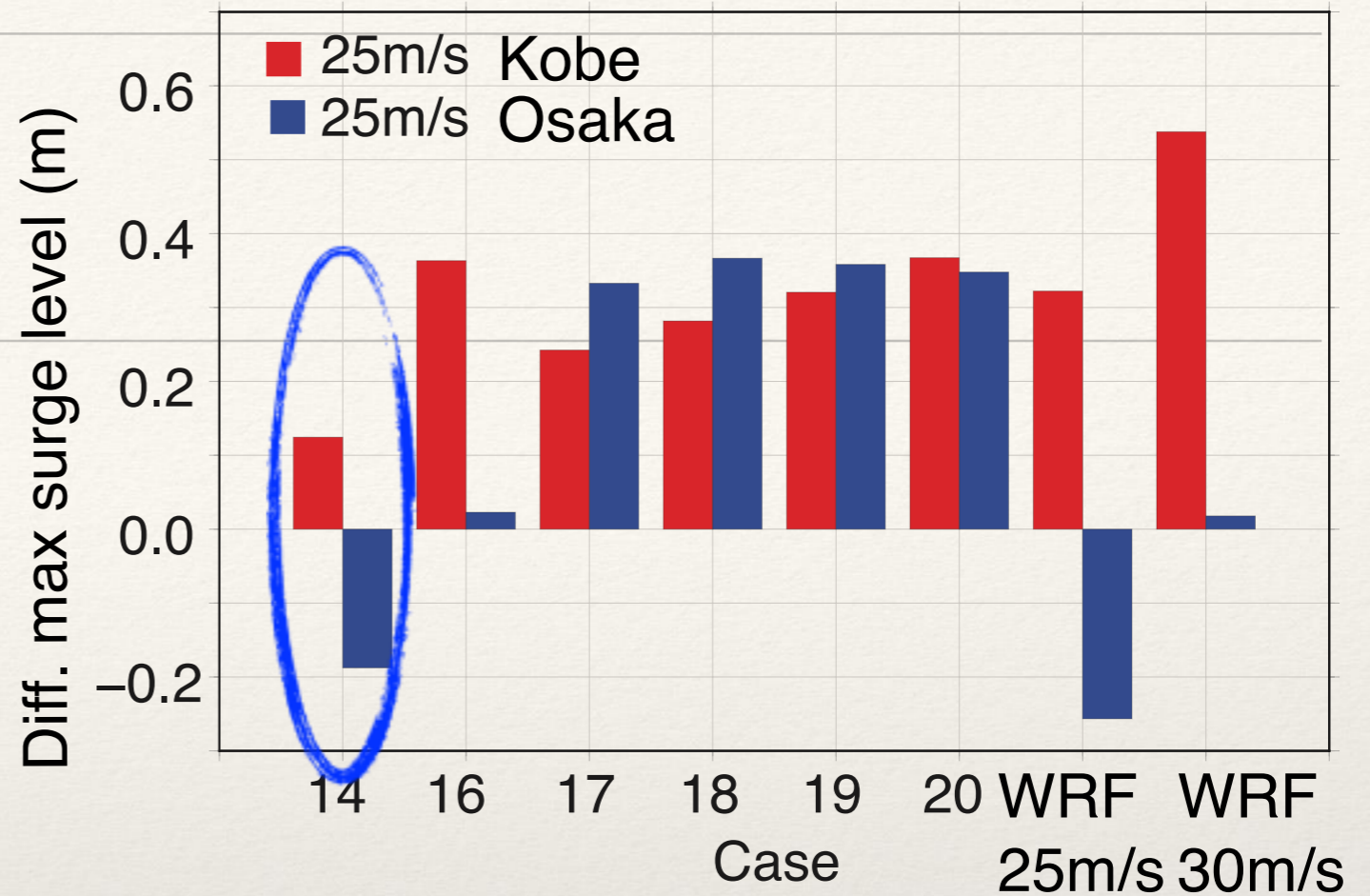
- ❖ Determine Wind limit based on difference between observed and calculated surge levels at Kobe and Osaka

❖ 25 m/s selected

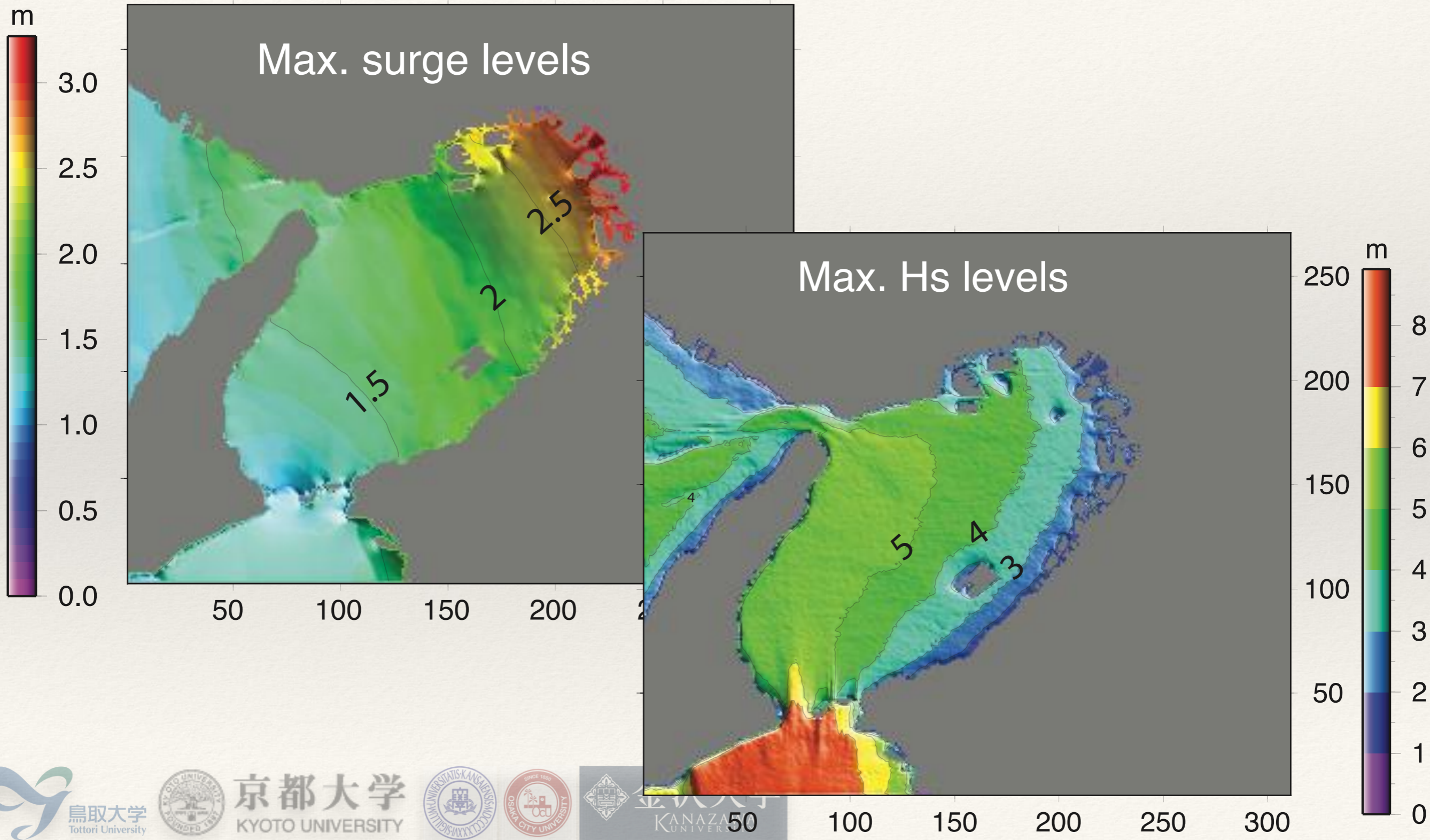


4. Estimating R_{max} by surge and H_s

- ❖ R_{max} before and after landfall at Osaka Bay = 20, 40, 60, 80, 100 km

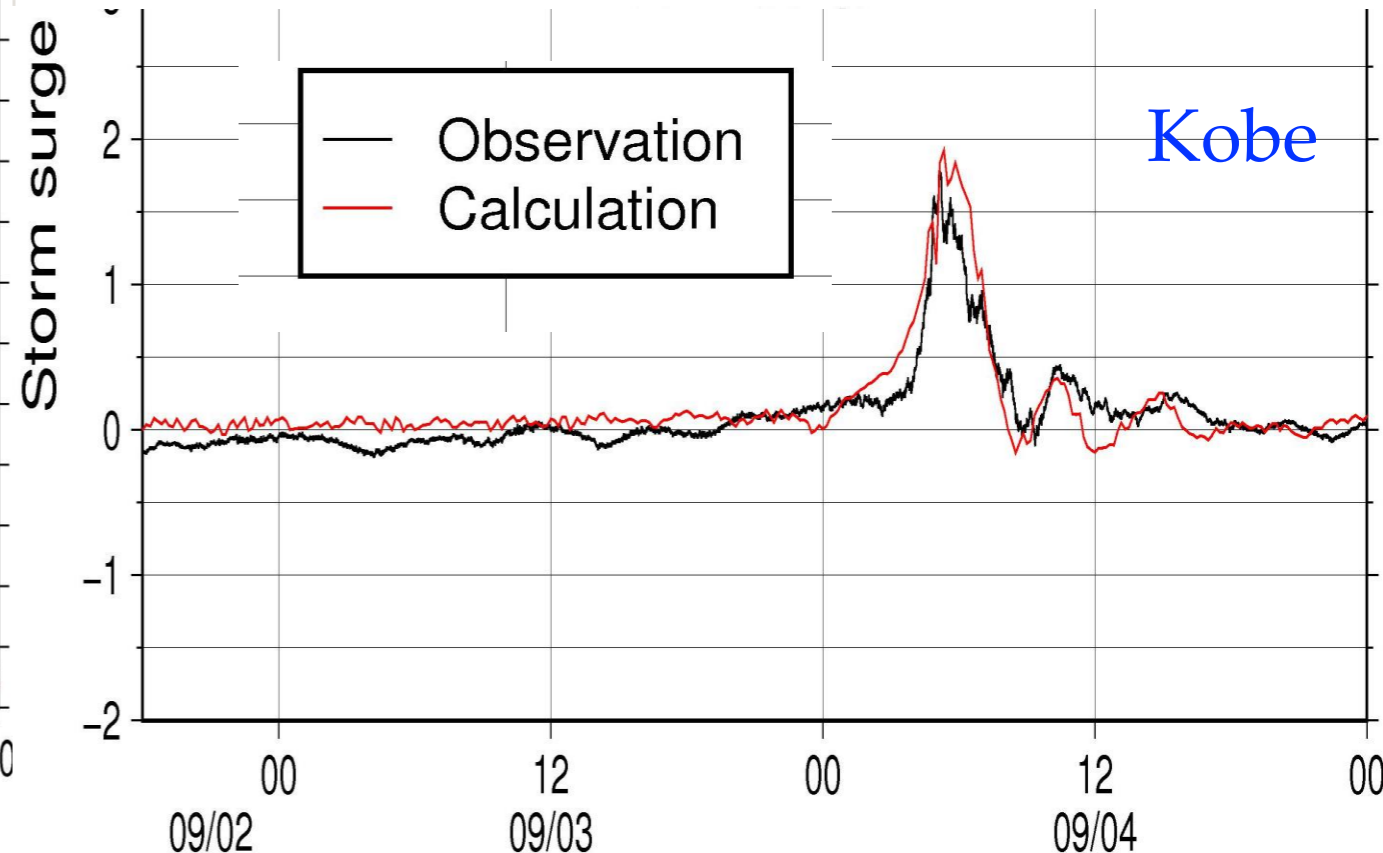
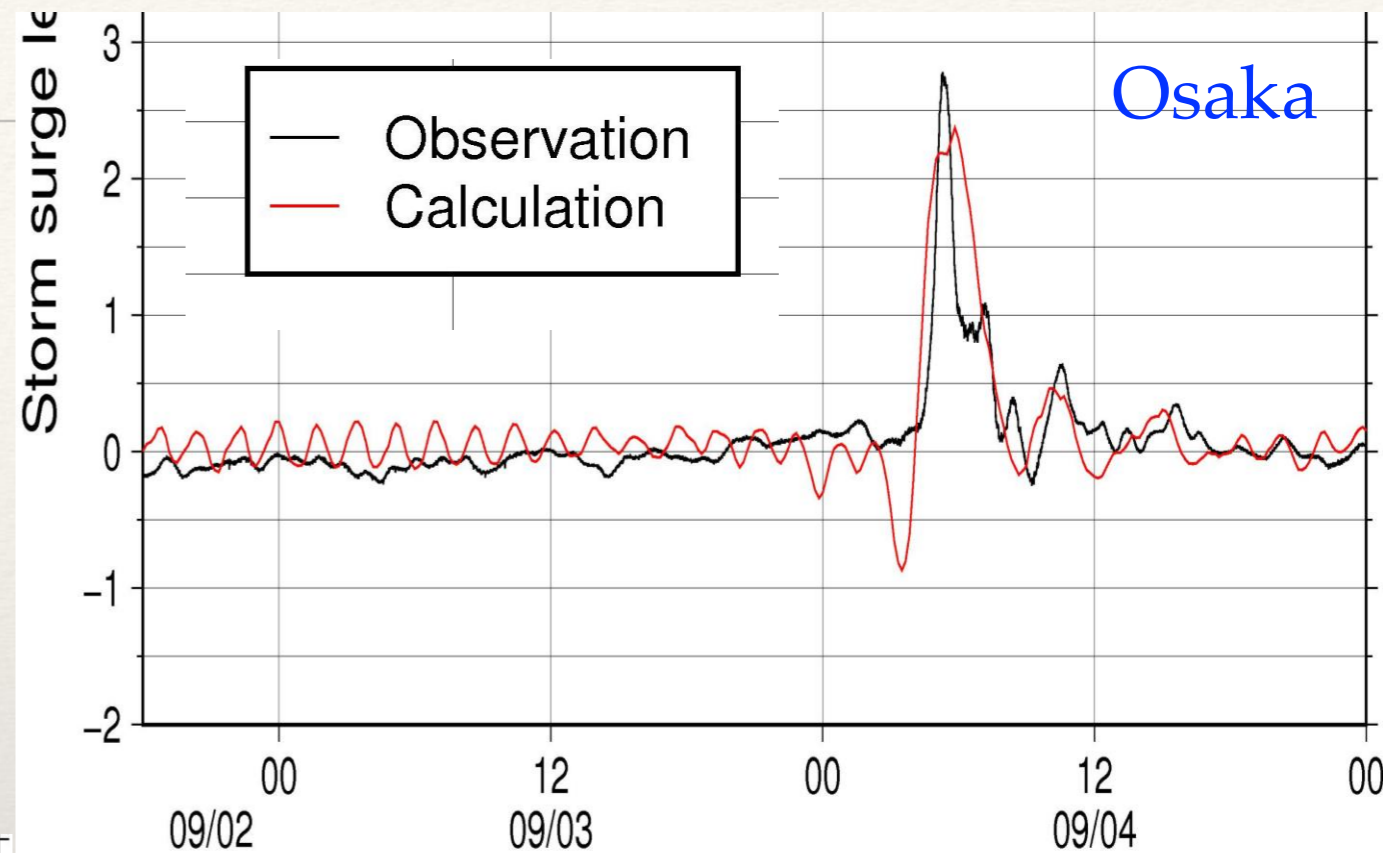
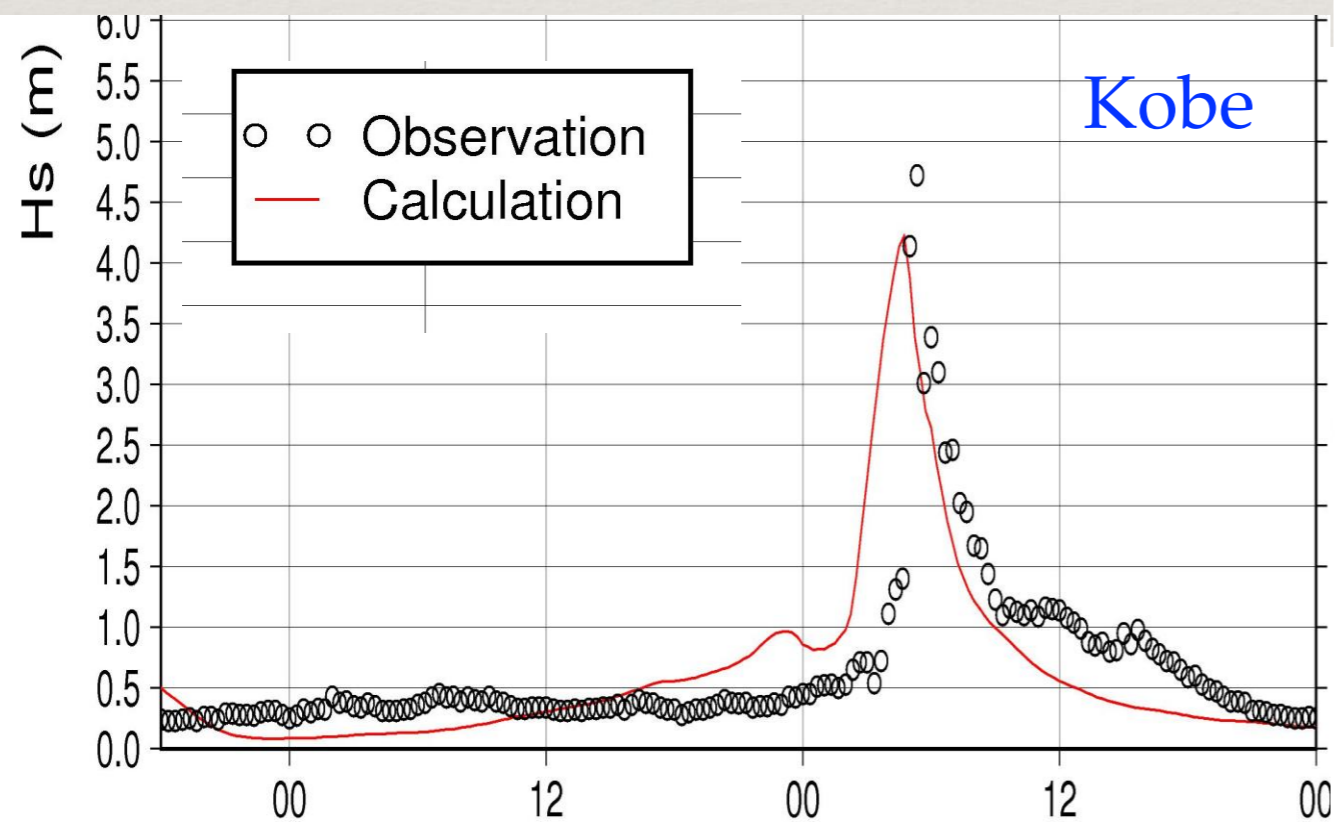


Tuned simulation of maximum surge and Hs

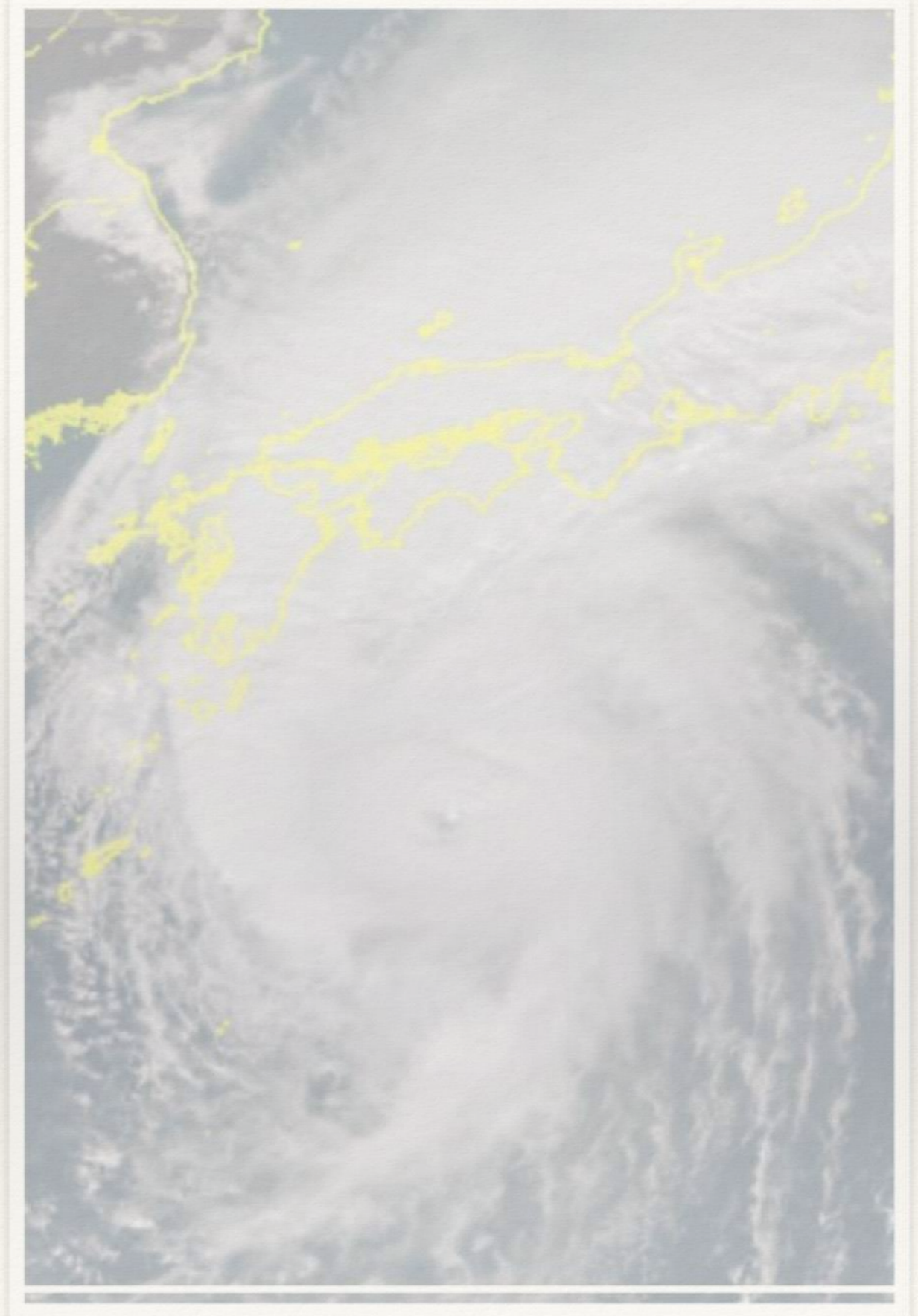


Tuned simulation of maximum surge and Hs

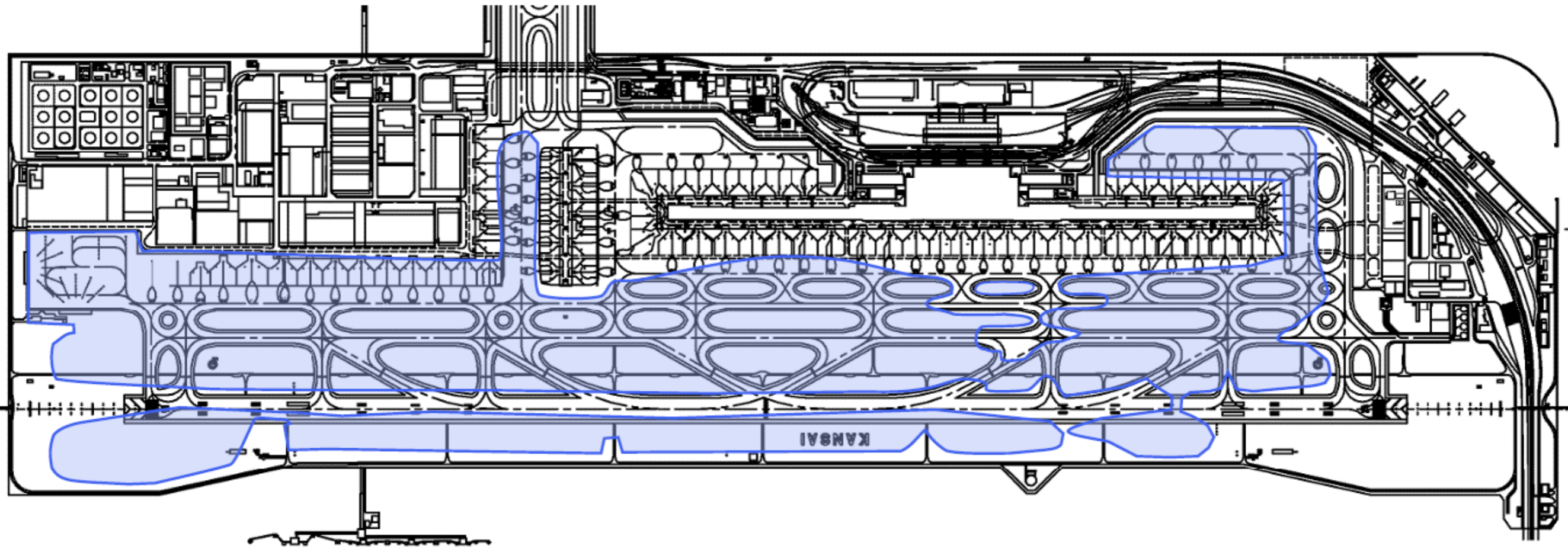
- ❖ A parametric wind and pressure model
 - ❖ $R_{max} = 150$ km in the bay,
- ❖ Coupled surge and wave model
 - ❖ wave dependent drag capped at 25 m/s,
 - ❖ on 90 m resolution



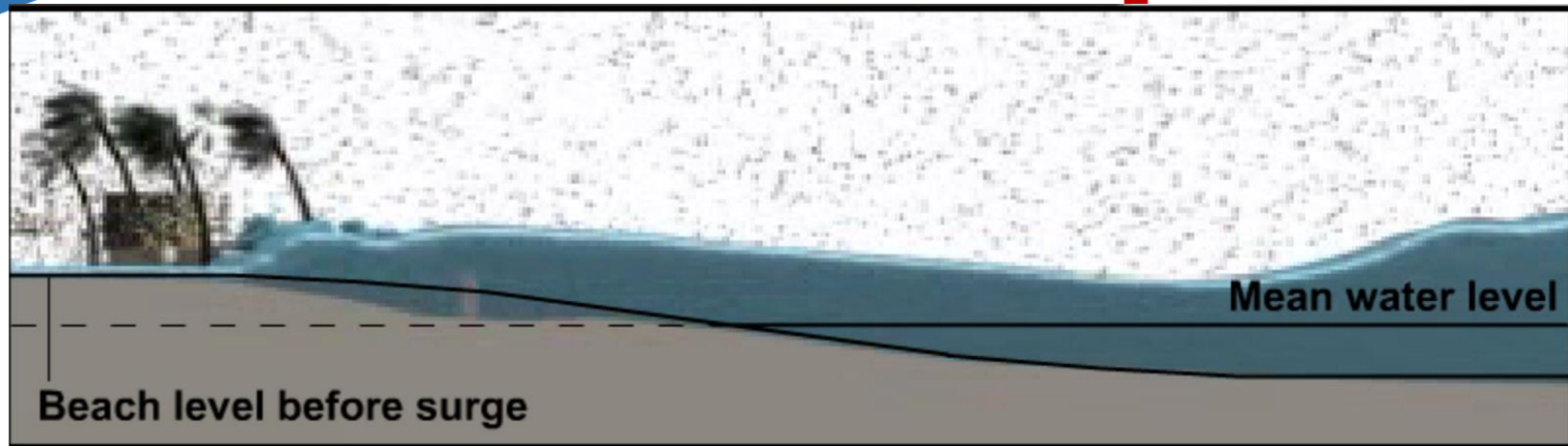
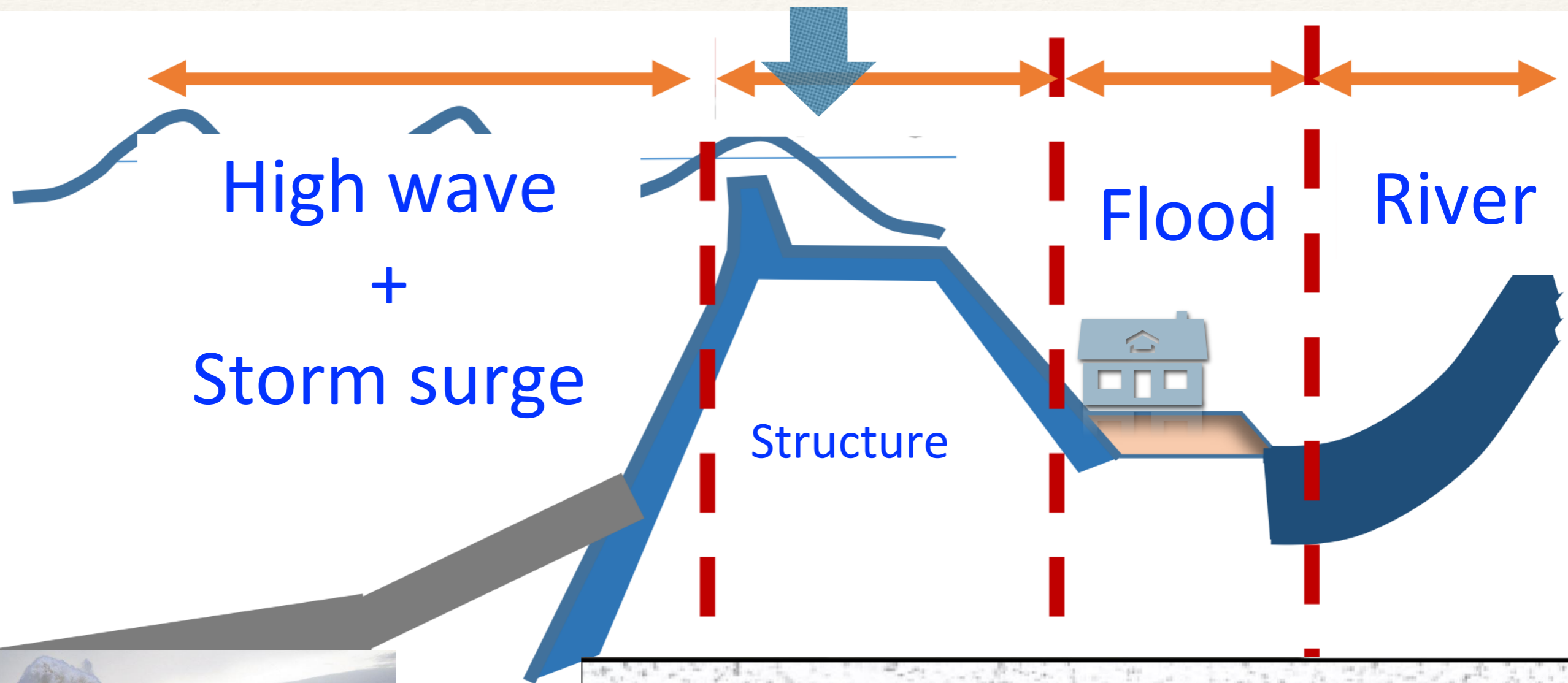
Flooding at Kansai Airport



Inundation area at Kansai Airport

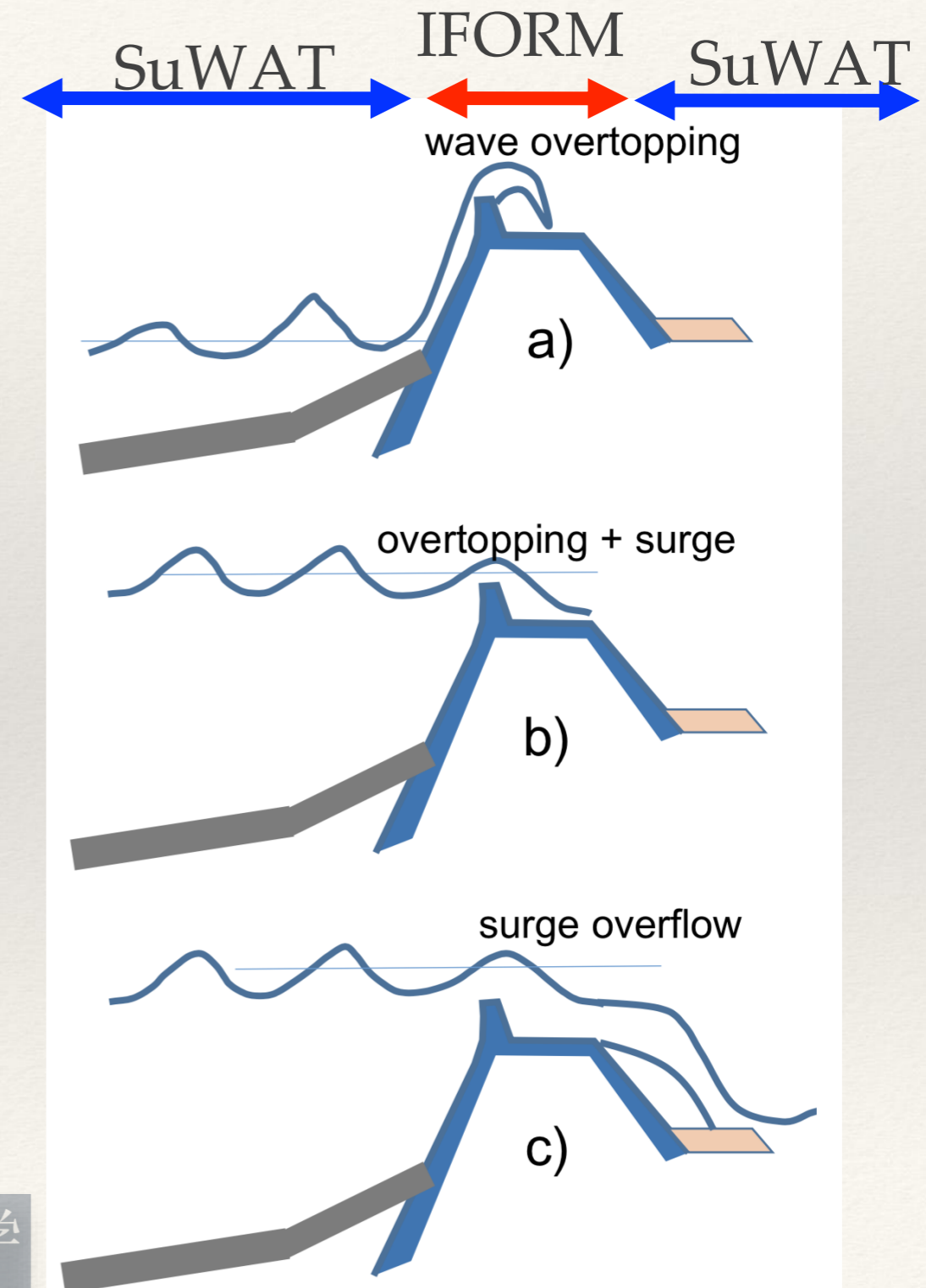


Flooding due to wave overtopping, runup and overflow

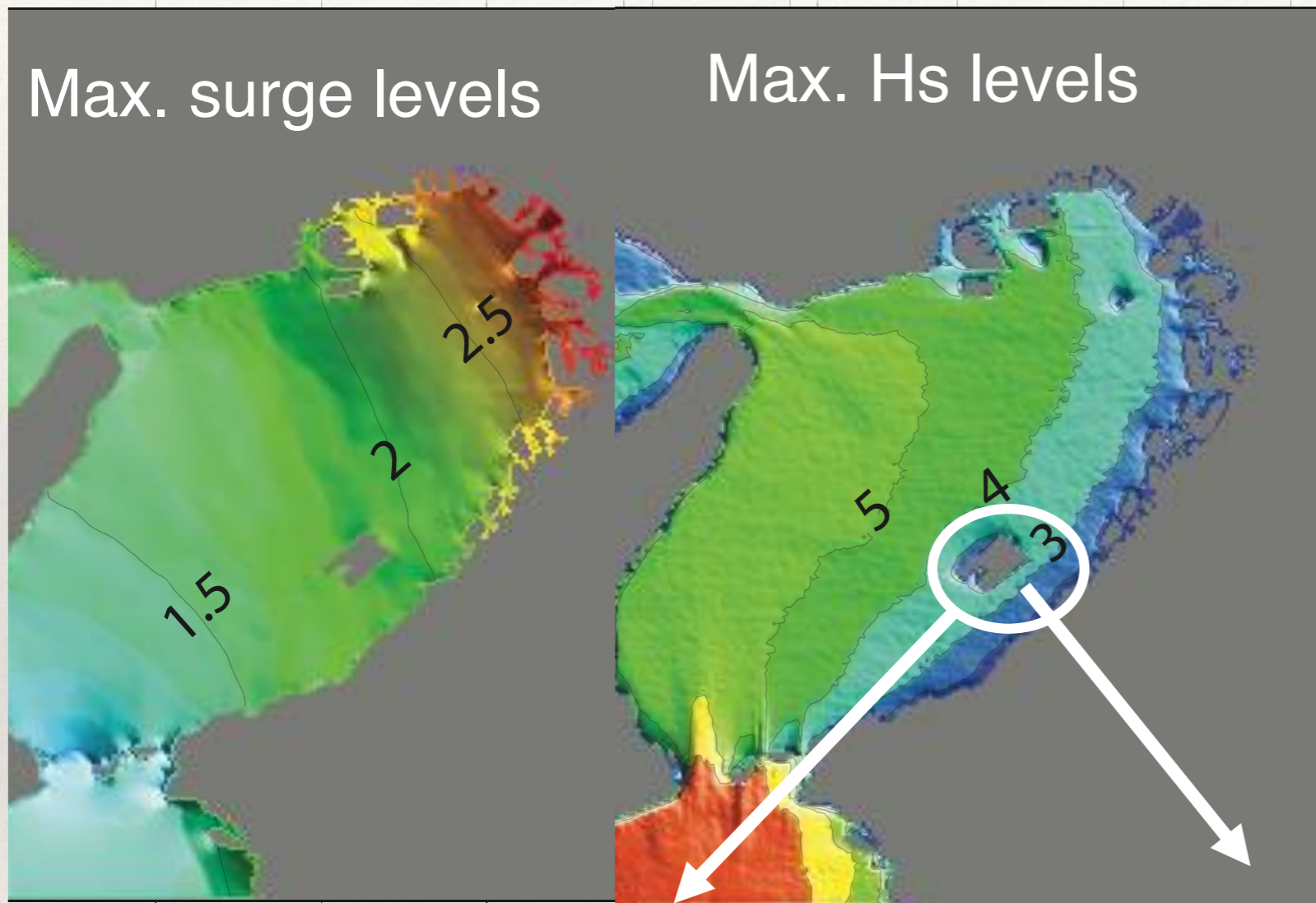


Flood modeling due to wave runup, overtopping and overflow at Kansai Int. Airport

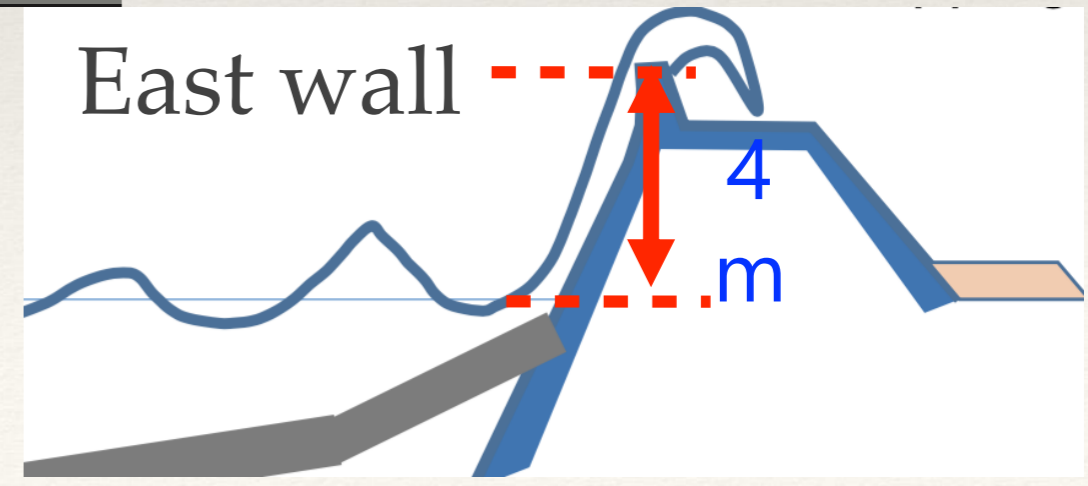
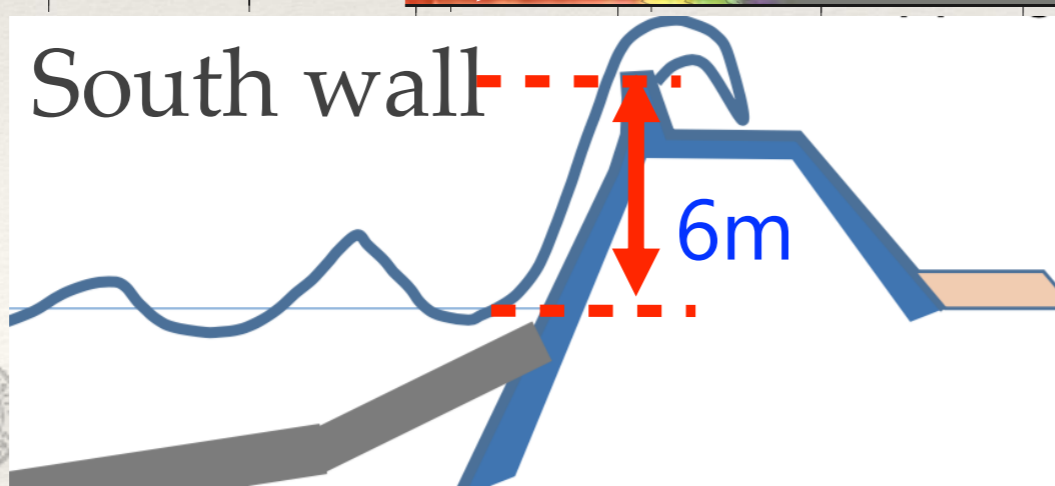
- ❖ Integrated model, SuWAT-IFORM (In preparation):
 - ❖ Coupled model of surge, wave and tide (SuWAT, Kim et al. 2015) and
 - ❖ Integrated Formula of wave Overtopping and Runup Modeling (IFORM, Mase et al. 2013, 2018)
- ❖ Calculation with rough bathymetry and breakwaters
- ❖ Recently secured information on flood was released, so further detailed simulations will be done



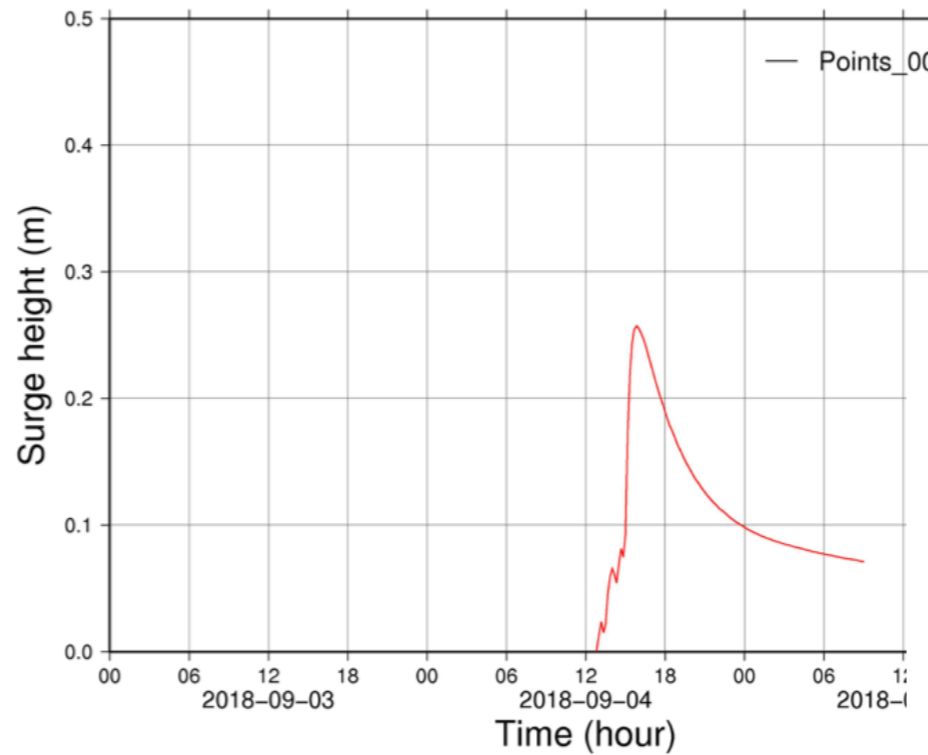
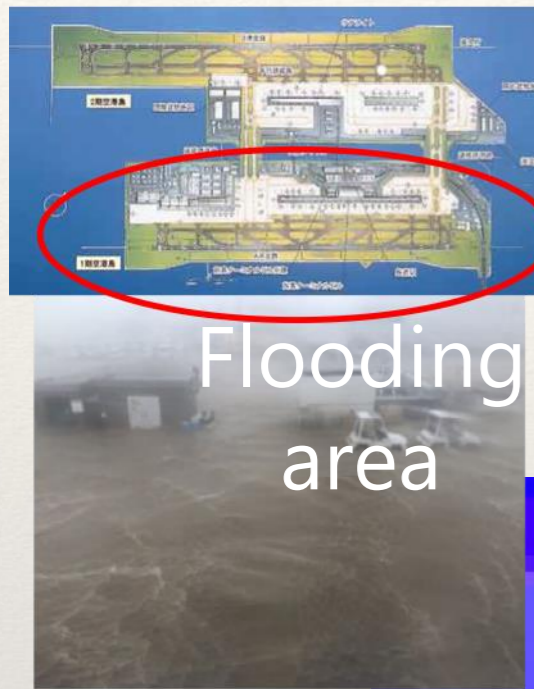
Modeling of inundation by surge and wave overtopping



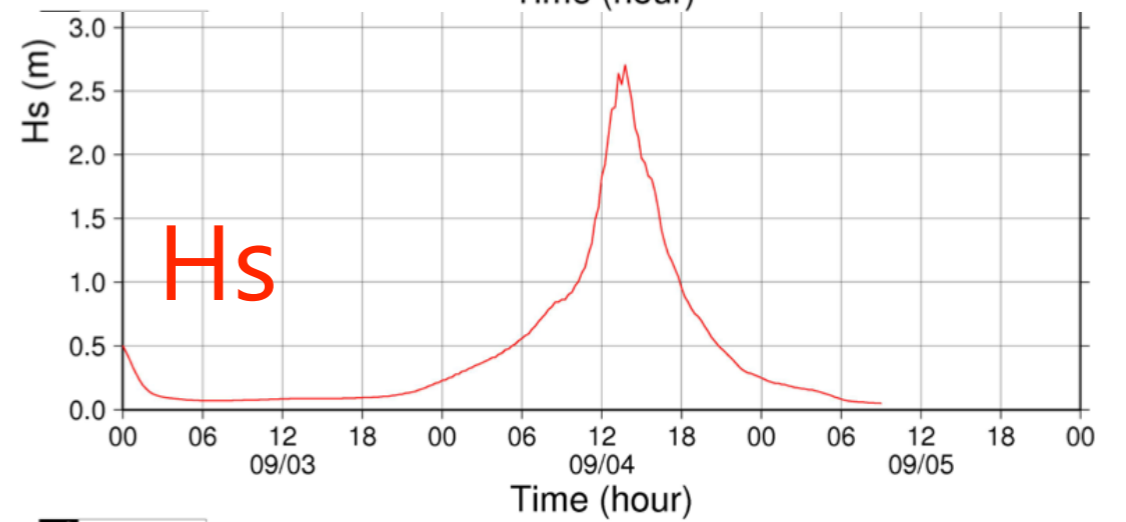
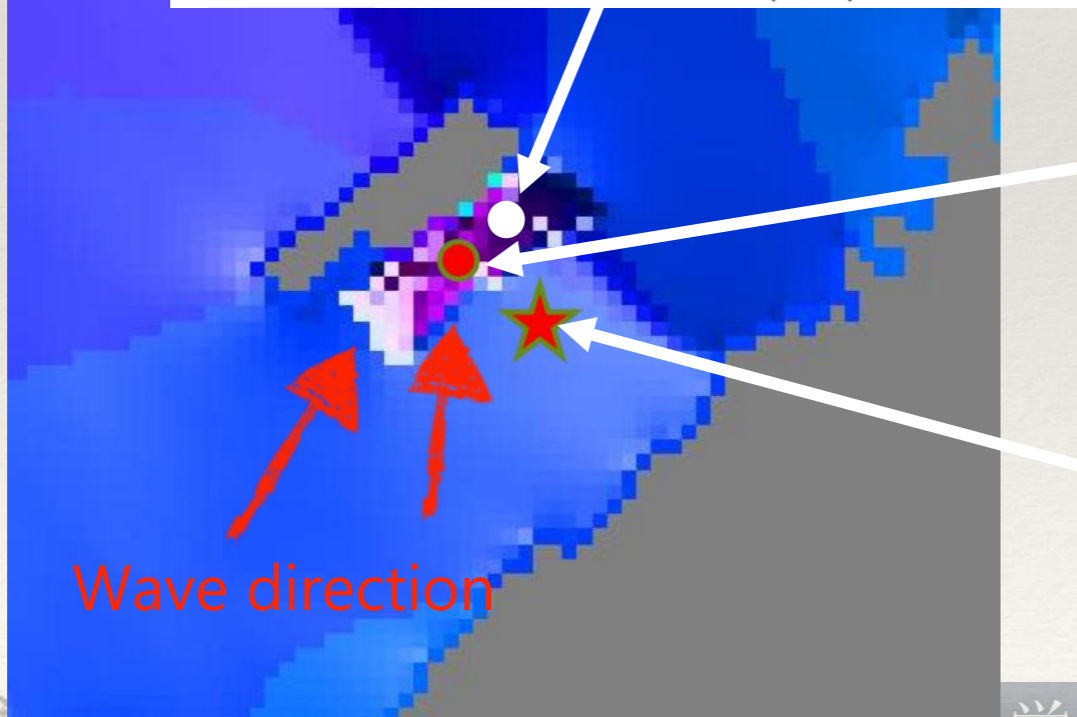
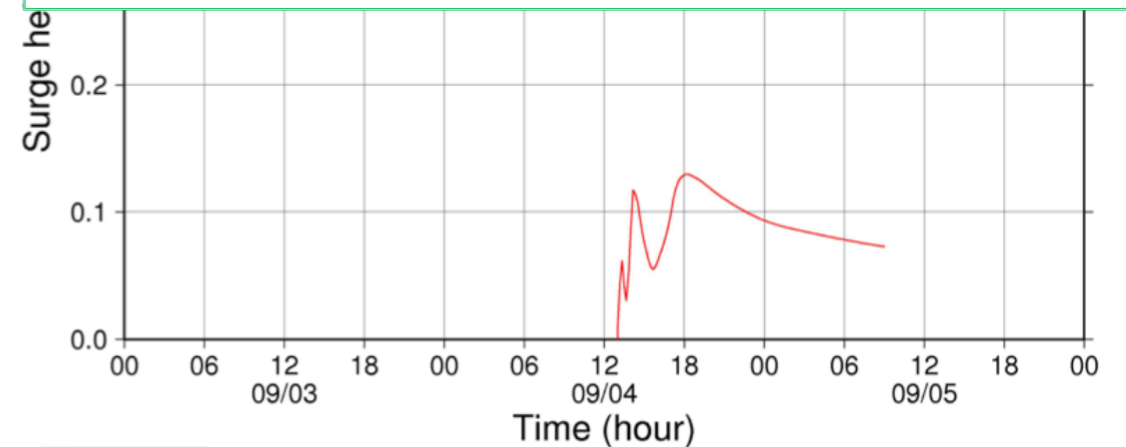
- ❖ Sea surface and wave levels (roughly) =
- ❖ on south wall
 - ❖ 1.7 m surge + 3.5 m Hs = 5.2 m
- ❖ on east wall
 - ❖ 1.7 m surge + 3.2 m Hs = 4.9 m



Flooding results due to wave runup and overtopping at Kansai Int. Airport



- A test run
- No consideration of overflow
- With walls with constant of 5 m height
- Only wave overtopping and runup
- Now studying with detailed information on walls and bathymetry



Summary

- ❖ Typhoon Jebi generated historical record-breaking waves and surges on the coast of Osaka Bay
 - ❖ max. surge level: 2.78 m
 - ❖ max. significant wave height : 4.72 m
- ❖ A symmetric & parametric wind and pressure model was used to reproduce Jebi's wind and pressure field
- ❖ Observed surges and waves were well simulated with the wave dependent drag capped at 25 m/s by SuWAT
- ❖ Flood due to wave overtopping, runup and overflow at Kansai Int. Airport was successfully simulated by SuWAT-IFORM .